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[0007] The insulations of stator windings that have been applied by winding have the disadvantage that their manufacture is time- and cost-intensive. In this context, special mention should be made of the winding process and impregnation process since they cannot be significantly accelerated any further because of the physical properties of the mica paper and impregnation resin. This manufacturing process is particularly prone to defects especially in the case of thick insulations, if the mica paper adapts insufficiently to the stator winding. In particular, an

1844 1845 1846 1847 1848 1849 1850 1851 1852 1853 1854 1855 1856 1857 1858 1859 1860 1861 1862 1863 1864 1865 1866 1867 1868 1869 1870 1871 1872 1873 1874 1875 1876 1877 1878 1879 1880 1881 1882 1883 1884 1885 1886 1887 1888 1889 1890 1891 1892 1893 1894 1895 1896 1897 1898 1899 1900 1901 1902 1903 1904 1905 1906 1907 1908 1909 1910 1911 1912 1913 1914 1915 1916 1917 1918 1919 1920 1921 1922 1923 1924 1925 1926 1927 1928 1929 1930 1931 1932 1933 1934 1935 1936 1937 1938 1939 1940 1941 1942 1943 1944 1945 1946 1947 1948 1949 1950 1951 1952 1953 1954 1955 1956 1957 1958 1959 1960 1961 1962 1963 1964 1965 1966 1967 1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990 1991 1992 1993 1994 1995 1996 1997 1998 1999 2000 2001 2002 2003 2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015 2016 2017 2018 2019 2020 2021 2022 2023 2024 2025 2026 2027 2028 2029 2030 2031 2032 2033 2034 2035 2036 2037 2038 2039 2040 2041 2042 2043 2044 2045 2046 2047 2048 2049 2050 2051 2052 2053 2054 2055 2056 2057 2058 2059 2060 2061 2062 2063 2064 2065 2066 2067 2068 2069 2070 2071 2072 2073 2074 2075 2076 2077 2078 2079 2080 2081 2082 2083 2084 2085 2086 2087 2088 2089 2090 2091 2092 2093 2094 2095 2096 2097 2098 2099 2100 2101 2102 2103 2104 2105 2106 2107 2108 2109 2110 2111 2112 2113 2114 2115 2116 2117 2118 2119 2120 2121 2122 2123 2124 2125 2126 2127 2128 2129 2130 2131 2132 2133 2134 2135 2136 2137 2138 2139 2140 2141 2142 2143 2144 2145 2146 2147 2148 2149 2150 2151 2152 2153 2154 2155 2156 2157 2158 2159 2160 2161 2162 2163 2164 2165 2166 2167 2168 2169 2170 2171 2172 2173 2174 2175 2176 2177 2178 2179 2180 2181 2182 2183 2184 2185 2186 2187 2188 2189 2190 2191 2192 2193 2194 2195 2196 2197 2198 2199 2200 2201 2202 2203 2204 2205 2206 2207 2208 2209 2210 2211 2212 2213 2214 2215 2216 2217 2218 2219 2220 2221 2222 2223 2224 2225 2226 2227 2228 2229 2230 2231 2232 2233 2234 2235 2236 2237 2238 2239 2240 2241 2242 2243 2244 2245 2246 2247 2248 2249 2250 2251 2252 2253 2254 2255 2256 2257 2258 2259 2260 2261 2262 2263 2264 2265 2266 2267 2268 2269 2270 2271 2272 2273 2274 2275 2276 2277 2278 2279 2280 2281 2282 2283 2284 2285 2286 2287 2288 2289 2290 2291 2292 2293 2294 2295 2296 2297 2298 2299 2300 2301 2302 2303 2304 2305 2306 2307 2308 2309 2310 2311 2312 2313 2314 2315 2316 2317 2318 2319 2320 2321 2322 2323 2324 2325 2326 2327 2328 2329 2330 2331 2332 2333 2334 2335 2336 2337 2338 2339 2340 2341 2342 2343 2344 2345 2346 2347 2348 2349 2350 2351 2352 2353 2354 2355 2356 2357 2358 2359 2360 2361 2362 2363 2364 2365 2366 2367 2368 2369 2370 2371 2372 2373 2374 2375 2376 2377 2378 2379 2380 2381 2382 2383 2384 2385 2386 2387 2388 2389 2390 2391 2392 2393 2394 2395 2396 2397 2398 2399 2400 2401 2402 2403 2404 2405 2406 2407 2408 2409 2410 2411 2412 2413 2414 2415 2416 2417 2418 2419 2420 2421 2422 2423 2424 2425 2426 2427 2428 2429 2430 2431 2432 2433 2434 2435 2436 2437 2438 2439 2440 2441 2442 2443 2444 2445 2446 2447 2448 2449 2450 2451 2452 2453 2454 2455 2456 2457 2458 2459 2460 2461 2462 2463 2464 2465 2466 2467 2468 2469 2470 2471 2472 2473 2474 2475 2476 2477 2478 2479 2480 2481 2482 2483 2484 2485 2486 2487 2488 2489 2490 2491 2492 2493 2494 2495 2496 2497 2498 2499 2500 2501 2502 2503 2504 2505 2506 2507 2508 2509 2510 2511 2512 2513 2514 2515 2516 2517 2518 2519 2520 2521 2522 2523 2524 2525 2526 2527 2528 2529 2530 2531 2532 2533 2534 2535 2536 2537 2538 2539 2540 2541 2542 2543 2544 2545 2546 2547 2548 2549 2550 2551 2552 2553 2554 2555 2556 2557 2558 2559 2560 2561 2562 2563 2564 2565 2566 2567 2568 2569 2570 2571 2572 2573 2574 2575 2576 2577 2578 2579 2580 2581 2582 2583 2584 2585 2586 2587 2588 2589 2590 2591 2592 2593 2594 2595 2596 2597 2598 2599 2600 2601 2602 2603 2604 2605 2606 2607 2608 2609 2610 2611 2612 2613 2614 2615 2616 2617 2618 2619 2620 2621 2622 2623 2624 2625 2626 2627 2628 2629 2630 2631 2632 2633 2634 2635 2636 2637 2638 2639 2640 2641 2642 2643 2644 2645 2646 2647 2648 2649 2650 2651 2652 2653 2654 2655 2656 2657 2658 2659 2660 2661 2

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[0009] Also known from cable technology are polymeric insulations applied to the cables using a hot shrink-on technique. This relates to prefabricated sleeves with a round cross-section of curing thermoplasts, elastomers, polyvinylidene fluoride, PVC, silicone elastomer or Teflon. After fabrication, these materials are stretched in their warm state and cooled. Once cooled, the material retains its stretched shape. This is accomplished, for example, because crystalline centers that fix the stretched macromolecules are formed. After repeated heating beyond the crystalline melting point, the crystalline zones are dissolved, whereby the macromolecules return to their unstretched state, and the insulation is in this way shrunk on. Also known are cold shrink-on sleeves that are mechanically stretched in their cold state. In the stretched state, these sleeves are pulled over a support

structure that holds the sleeves permanently in the stretched state. Once the sleeves have been pushed and fixed over the components to be insulated, the support structure is removed in a suitable manner, for example, by pulling a spiral, perforated support structure out. But such shrink-on techniques cannot be used for stator windings with a rectangular cross-section since the sleeves with their round cross-section easily tear along the edges of the rectangular conductors, either immediately after shrinking or after being strained briefly while the electrical machine is operated, because of the thermal and mechanical stresses.

[0010] Even while the stator windings are being manufactured, especially during the bending and handling of the conductors, particularly during installation into the stator, the insulation must be able to bear a significant high mechanical stress which could damage the insulation of the stator windings. The insulation of the stator winding conductors is also exposed to a combined stress during operation of the electrical machine. On the one hand, the insulation is dielectrically stressed between the conductor, to which a high voltage is applied, and the stator, by a resulting electrical field. On the other hand, the heat generated in the conductor exposes the insulation to a thermal alternating stress, whereby a high temperature gradient is present in the insulation while the machine passes through the respective operating states. Because the materials involved expand differently, mechanical alternating stresses also occur. This results both in a shearing stress of the bond between conductor and insulation and a risk of abrasion at the interface between insulation and slot wall of the stator. Because of these high stresses, the insulation of the stator windings may tear, resulting in a short circuit. Consequently, the entire electrical machine will fail, and the repair will be time- and cost-intensive.

#### Description of the Invention

[0011] This is the starting point for the invention. The invention, as characterized in the claims, is based on the objective of creating a process for

insulating stator windings for rotating electrical machines, whereby insulated stator windings are produced that ensure the insulation of the stator winding over the intended life span of the electrical machine.

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[0012] This objective is realized by the method according to the characteristics of independent Claim 1.

[0013] The method according to the invention for producing an insulated stator winding for rotating electrical machines, in particular, direct current machines and alternating current machines, where said insulated stator winding is constructed of at least one electrically conductive conductor bar with an essentially rectangular cross-section, whereby at least one electrically insulating shrink-on sleeve with an essentially rectangular cross-section is applied to the periphery of the conductor bar and shrunk onto the conductor bar, has the advantage that the shrinking-on of an insulated stator winding produces an insulated stator winding that ensures an advantageous insulation. This is the case particularly because the electrically insulating shrink-on sleeve always hugs the conductor bar at each point without forming wrinkles or voids, whereby the edges of the shrink-on sleeve come to rest against the edges of the conductor bar. This prevents a potential tearing of the shrink-on sleeve at the edges. The prefabrication of the shrink-on sleeve with the known shaping processes (extrusion, injection molding) also ensures, when combined with testing of the electrical components prior to assembly, an optimum insulation quality. Because of its defined thickness, the shrink-on sleeve also encloses the conductor bar in the required manner uniformly at each point of its periphery in order to ensure a suitable electrical and mechanical insulation. This ensures that the insulated stator winding has sufficient insulation over the intended life span of the electrical machine.

[0014] Because there are only a few, simple process steps, an insulated stator winding is manufactured in a time- and cost-efficient manner, whereby both straight and pre-bent conductor bars can be insulated, so that the conductor bar can be bent into its final shape either prior to or after the insulation is applied.

[0015] It was found to be advantageous that the shrink-on sleeve is mechanically dilated in its cold state and applied to the outer periphery of a support device, in particular, a support sleeve, before the support sleeve that has been surrounded with the shrink-on sleeve is pulled over the conductor bar, whereby the support sleeve is larger than the conductor in order to facilitate the application of the shrink-on sleeve onto the conductor bar.

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[0016] The contact of the shrink-on sleeve with the conductor bar is ensured in that, after application of the support sleeve surrounded by the shrink-on sleeve, the support sleeve between the shrink-on sleeve and the conductor bar is removed, in particular by opening the shrink-on sleeve helically, so that the shrink-on sleeve contracts around the conductor bar.

[0017] Alternatively, the contact of the shrink-on sleeve with the conductor bar can be achieved in that the support sleeve contains a meltable polymer, whereby, after the support sleeve surrounded by the shrink-on sleeve has been applied to the conductor bar, the support sleeve is brought to melting by introducing heat, so that the dilated shrink-on sleeve is able to relax and starts to hug the conductor bar.

The molten support sleeve hereby advantageously functions as an adhesive and sealing mass. If the support sleeve is constructed in a conductive manner, the molten support sleeve also assumes the function of the internal corona shielding.

[0018] It has also been found to be advantageous to use a shrink-on sleeve of a heat-shrinking material that is mechanically dilated in the warm state and is cooled in this dilated state. Specific material properties ensure that part of this dilation is maintained in the cold state. In this state, the shrink-on sleeve is pulled over the conductor bar, whereby the shrink-on sleeve is then shrunk, under application of heat, onto the conductor bar so that no further devices are necessary for insulation.

[0019] Alternatively, the assembly may take place by using compressed air for dilating the sleeve.

[0020] It is also advantageous that the shrink-on sleeve is constructed of several layers with different properties around the periphery of the conductor bar,

whereby the layers provide the internal corona shielding, the main insulation, the slot corona shielding, and the yoke corona shielding.

[0021] A preferred mechanical connection between the conductor bar and the shrink-on sleeve can be achieved if the shrink-on sleeve has at its contact surfaces with the conductor bar a thermally stable adhesive. This also prevents the formation of voids, so that the thermal conductivity is improved and electrical void discharges are avoided, which is especially an advantage for variations in which no internal corona shielding is used.

[0022] If the shrink-on sleeve is constructed of an extruded elastomer sleeve, it can be constructed continuously, on the one hand, in an advantageous manner, and, on the other hand, can be adjusted to different bar geometries. The elastomer insulation furthermore prevents tearing of the insulation during the bending. The present invention uses the high elasticity of the elastomer while maintaining the ability to withstand high thermal and electrical stresses. For higher thermal stresses a silicone elastomer is used advantageously.

[0023] In a particularly preferred method, the conductor bars are only brought into their final shape after being encased with the elastomer. The bending of the involutes greatly stretches the applied insulation. The use of elastomer according to the invention is hereby found to be particularly advantageous, since it reduces or even completely avoids mechanical, electrical or thermal injury to the insulation that is being stressed by bending.

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**Brief Description of Drawings**

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[0024] The invention is described in more detail below with reference to the drawings, using exemplary embodiments.

[0025] Fig. 1a shows a cross-section through an insulated stator winding with conductor bar and shrink-on sleeve;

[0026] Fig. 1b shows a cross-section through an insulated stator winding with conductor bar, support sleeve, and shrink-on sleeve (prior to shrinking);

[0027] Fig. 2 shows a partial section of the side view of Fig. 1b; and,  
[0028] Fig. 3 shows a device for bending the insulated conductor bars.  
[0029] The figures only show the elements and components essential for understanding the invention. The shown methods and devices according to the invention therefore can be supplemented in many ways or can be modified in a manner obvious to one skilled in the art, without abandoning or changing the concept of the invention.

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#### Ways of Executing the Invention

[0030] Fig. 1a shows a cross-section through an insulated stator winding 60. A rectangular conductor bar 2 is hereby surrounded by a shrink-on sleeve 64. The conductor bars themselves usually are constructed of a bundle of individual, insulated conductors. In Roebel-transposed conductor bars, the individual conductors are in part twisted around each other, while in non-Roebel-transposed conductor bars the individual conductors extend parallel to each other without twisting. In the invention, conductor bars with individual conductors that have a round cross-section can be used. However, the application of the method according to the invention for conductor bars with individual conductors with a rectangular cross-section is particularly advantageous. When using rectangular cross-sections, the advantages of the invention are also obtained when the cross-sections of the individual conductors and/or of the conductor bar deviate slightly from the rectangular shape. If the conductor bar is constructed of individual conductors, it is advantageous that these are temporarily connected to each other in order to enable a uniform and cavity-free encasing of the conductor bar with the main insulation, for example, by temporarily bonding the individual conductors with an elastic material or an adhesive with low mechanical strength against shearing forces, so that later bending is not impeded. Alternatively, an adhesive that loses its bending power during moderate heating (e.g., before bending) and thus promotes the bending process.



[0031] The shrink-on sleeve 64 shown in Fig. 1a preferably is manufactured from a hot-shrinking material. The material is stretched in its warm state and is then kept partially or completely in its stretched state through a subsequent cooling process without subjecting the sleeve to any further mechanical influences. During heating, the sleeve returns to its rubber-elastic behavior and shrinks onto the bar when subjected to heat.

[0032] Fig. 1b shows a cross-section through an insulated stator winding 60 that is constructed of an electrically conductive, potentially Roebel-transposed conductor bar 2 that has a rectangular cross-section and is encased by a support sleeve 62 with an extra width 65 in relation to the conductor cross-section, and which supports the electrically insulating shrink-on sleeve 64 with its rectangular cross-section, also with an extra width in relation to the conductor cross-section, in order to permit an easy assembly, i.e., a sliding-on of the sleeve. It is also preferred here that both the internal cross-section as well as the external cross-section of the shrink-on sleeve are constructed rectangular. The shrink-on sleeve shown here is preferably manufactured from cold-shrinking material.

[0033] In both of the embodiments shown in Fig. 1a and b, the shrink-on sleeve can be manufactured from a hot-shrinking or cold-shrinking material. The shrink-on sleeve preferably has a rectangular cross-section that matches with the cross-section proportions of the conductor bar, whereby the internal cross-section of the completely shrunk sleeve should be smaller than the conductor cross-section in order to ensure optimum contact with the conductor cross-section. It is especially preferred that both the internal and external cross-section of the shrink-on sleeve are rectangular.

[0034] It is preferred that an elastomer is used as a material for the shrink-on sleeve. The elastomer is characterized by high elasticity. It also has a high electrical and thermal stability. In particular for thermally highly stressed machines it is preferred that silicone elastomers are used. Especially the advantageous use of elastomer (in contrast to other materials) permits the use of

injection molding processes and fulfills the high requirements for material resistance and mechanical flexibility. The elastomers may be cold- or hot-curing types. The curing for cold-curing types is initiated, for example, by mixing two components, whereby one of the components contains a curing agent. In the case of hot-curing types, the elastomer can be heated already in the injection mold or the extruder. During the extrusion, the curing can also be initiated after the exit from the extruder, for example, with hot air.

[0035] The material properties of the main insulation can be adjusted in such a way by adding active (e.g., silicic acid) and passive (e.g., quartz sand) fillers that they fulfill the respective mechanical requirements of the electrical machines into which the stator windings provided with the main insulation are installed.

[0036] In some applications, it is preferred that the conductor bars are provided with slot corona shielding and termination (yoke corona shielding) as well, if applicable, with an internal corona shielding. The internal corona shielding of a stator winding is usually a conductive material layer located between main insulation and conductor bar. It enables a defined potential coating around the conductor bar and prevents electrical discharges that can be caused by voids between the conductor bar and the main insulation. The slot or external corona shielding of a stator winding usually is a conductive material layer located between the main insulation and the stator slot. The external corona shielding, which again creates a defined potential layer, is supposed to prevent electrical discharges that can be caused, for example, by varying distances of the high potential insulated conductor bar from the grounded stator nut. The direction (yoke corona shielding) usually prevents electrical discharges at the slot exit of a conductor bar. Options for applying such protective layers within the scope of this invention include, for example, conductive or semi-conductive elastomer-based finishes, suitable tapes (possibly self-fusing), which can be cured by irradiation or heat. Alternatively, cold- or heat-shrink-on sleeves (for example, for bars) or cuffs (for example, for coils) can be used. When using shrink-on sleeves or cuffs for the internal corona

shielding, these may be provided advantageously on their inside with a flowable, plastic material to fill the voids on the surface of the conductor bar. This is basically also possible for an external corona shielding.

[0037] In another preferred embodiment of the method, internal corona shielding, main insulation, and/or external corona shielding are applied in the form of several shrink-on sleeves or one shrink-on sleeve consisting of several layers.

[0038] Fig. 2 shows the insulated stator winding 60, whereby the shrink-on sleeve 64 is shown in a partial section view. The shrink-on sleeve 64 surrounds the support sleeve 62 that is provided with helically arranged perforations 66 for removing the support sleeve.

[0039] In order to produce the insulated stator winding 60, the shrink-on sleeve 64 is mechanically dilated in its cold state and is applied in this dilated state around the outer periphery of the support sleeve 62 that holds the shrink-on sleeve 64 in the stretched state. Then the support sleeve 62 that is surrounded by the shrink-on sleeve 64 is pulled over the conductor bar 2 and, as required, is fixed so that the periphery of the conductor bar 2 is surrounded by the support sleeve 62. After applying the support sleeve 62 that is surrounded by the shrink-on sleeve 64 onto the conductor bar 2, the support sleeve 62 between the shrink-on sleeve 64 and the conductor bar 2 is removed by helically opening the support sleeve 62 along helically arranged perforations 66. The stretched shrink-on sleeve 64 then relaxes and then hugs the conductor bar 2. The conductor bar 2 insulated in this manner is bent with a bending device into the shape suitable for the stator, whereby the insulated conductor bar 2 can also be bent directly in the stator if it is sufficiently flexible.

[0040] Alternatively, the support sleeve 62 is not constructed as a perforated spiral but consists of a meltable polymer, for example, a thermoplast or duroplast, in the bi-stage state. By introducing heat, the melting of the support sleeve is initiated so that the stretched sleeve is able to relax and hugs the conductor. After solidifying, the molten polymer also functions as an adhesive mass or sealing mass

for filling any voids. If the polymer is conductive, it is also able to assume the function of the internal corona shielding.

[0041] Fig. 3 shows a bending device that has been modified from the state of the art. The insulated conductor bars are placed into the gripping jaws 18 of the bending device and are brought there into their final shape by moving the gripping jaws 18 in relation to the radial tools 20. Between the radial tools 20 and the insulating layer 4 of the conductor bar 2 that has been produced from the shrink-on sleeve 64, a protective layer 22 is provided that distributes the pressure generated at the radial tools over the surface and in this way prevents an excessive pinching of the insulation layer 4. The uniformly distributed mechanical stress on the elastomer insulation layer prevents damage to the insulation layer. The bending of the involute causes very high tensile forces in the insulation layer 4 that can be absorbed by the elastomer used for the shrink-on sleeve 64 without damaging it, however.

[0042] If the conductor bar is constructed of a bundle of individual conductors, the bending of conductor bars already provided with the main insulation causes both a relative movement of the individual conductors against each other as well as a relative movement of the individual conductors at the surface of the conductor bar against the main insulation. It is advantageous that the interface between conductor bar and main insulation has properties that enable a shifting of the individual conductors against the main insulation with reduced friction. This may be achieved, for example, by treating the conductor bar with separating agents. The occurrence of gaps due to this relative movement at the interface to the conductor is meaningless if an internal corona shielding connected tightly with the main insulation is used in this area. Without internal corona shielding, the shifting is, in most cases, uncritical because the field is reduced in the bend area (following the termination).

[0043] When using an internal corona shielding, it is advantageous that it has good adhesion in relation to the main insulation, but has a lesser adhesion in

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**[0044]** As is obvious from the previous description, many modifications and changes of the embodiment described here can be made without exceeding the scope of the invention.

~~List of Reference Numbers~~

2	Conductor bar
4	Insulation layer
18	Gripping jaws
20	Radial tool
22	Protective layer
60	Insulated stator winding
62	Support sleeve
64	Shrink-on sleeve
65	Extra width
66	Perforation

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